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INTERSTATE COUNCIL FOR STANDARDIZATION, METROLOGY AND CERTIFICATION
(ISC)

**EN 1891-
2014**

▪

(EN 1891:1998, IDT)



2015

1.0-92 «
 1.2-2009 «
 -7
 -320 « »
 14 2014 . 72-)

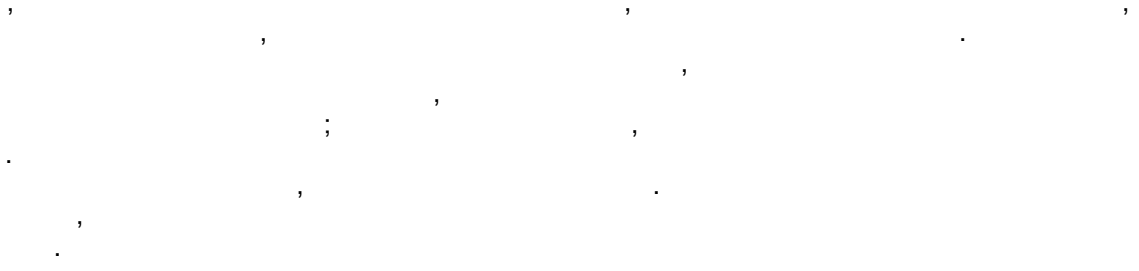
(3166) 004-97	(3166) 004-97	
	AM BY KG MD RU	-

4 1822- EN 1891-2014 26
 1 2015 .

5 EN 1891:1998
 Personal protective equipment for the prevention of falls from a height - Low stretch kernmantel ropes
 () .

1891-2012

6
 « » ,
 « » . ()
 « » .



Occupational safety standards system Personal protective equipment against falls from a height Low stretch kernmantel ropes. General technical requirements. Test methods

- 2015-12-01

1

8.5 16

1

2

EN 892.

2

EN 364, Personal protective equipment against falls from a height — Test methods ()

EN 365, Personal protective equipment against falls from a height — General requirements for instructions for use, maintenance, periodic examination, repair, marking and packaging

EN 701, Fibre ropes for general service - General specification ()

EN 919, Fibre ropes for general service - Determination of certain physical and mechanical properties ()

EN 892, Mountaineering equipment - Dynamic mountaineering ropes - Safety requirements and test methods ()

3

3.1 (low stretch kernmantel): (),

3.2 (access):

3.3 (work positioning):

3.4 A (type A ropes):

3.5 (type)::

4

4.1

4.2 *D* 195 °C. 5.3,

4.3 8,5 16

4.4 1,2 5.4. S_s S_s 5.5. *D*, 5.3, 12, 1 16 12 20 + 10 (- 9), + 5 (- 12).

4.5 *I/* 5.5.6.

4.6 *R* *R* 5.6 5 %.

4.7 *R* 5.7.

5.8. 1000

4.8 5.8 S_p

$$S = \frac{\left(\frac{D}{2}\right)^2 - \left(\frac{D-2}{2}\right)^2}{\left(\frac{D}{2}\right)^2} \cdot 100\%$$

5 - 4D 4 100%
kJ mtn *

S -
D - 5.3.

4.9

5.8

$$= 12 - 37 \cdot 100\%$$

$$= \text{mm} \frac{4S}{* , 1} \frac{\%}{J^9}$$

$$v. - \min \frac{10}{(D) -} \cdot 100\%,$$

$$(2)$$

$$C_{\min} = \frac{40}{D^2} \cdot 100\%$$

D - 5.3.

4.10

5.9.4

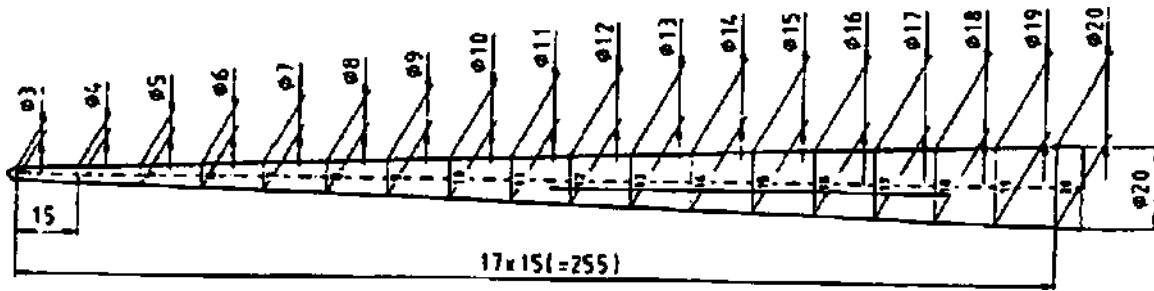
F

6 .

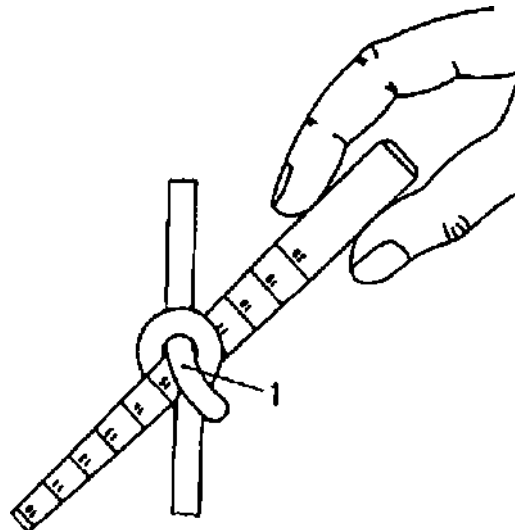
4.11

5.9.5

4.12					
4.12.1	919 (4.1, 5.1,	6,	8.1,8.2, 8.5	9.5)
22		18	-		
4.12.2					
	5.10				3
	15' 5		12*05		
	(,)	,	
5					
5.1					
5.2					
	24		72	10 %	
	(65 ± 5) %		(23 ± 5) °C.	(20 ± 2)'	
5.3	<i>D</i>				
5.3.1					3000
5.3.2					
5.3.2.1					
5.3.2.2				(10 ± 0,1)	
5.3.2.3	1300				
			5.3.2.2	(60 ± 15)	
				90°	
			300		
		(50 ± 1)			
5.3.3	<i>D</i>				
			8,5	16	0,1
5.4					
5.4.1					3000
5.4.2					
5.4.2.1					
(250 ± 50)					
5.4.2.2					
5.4.2.3				(10 ± 0,1)	
5.4.2.4			5.4.2.3	(60 ± 15)	
5.4.2.5		(1 ± 0,1)			
	0,5				
(1).				
(2).				



1 -



1 - точка измерения

2 -

5.4.3
5.4.3.1
5.4.3.2

= _____ 5.3.3

5.5
5.5.1

S_s

3,

5.5.2

(22501 10)

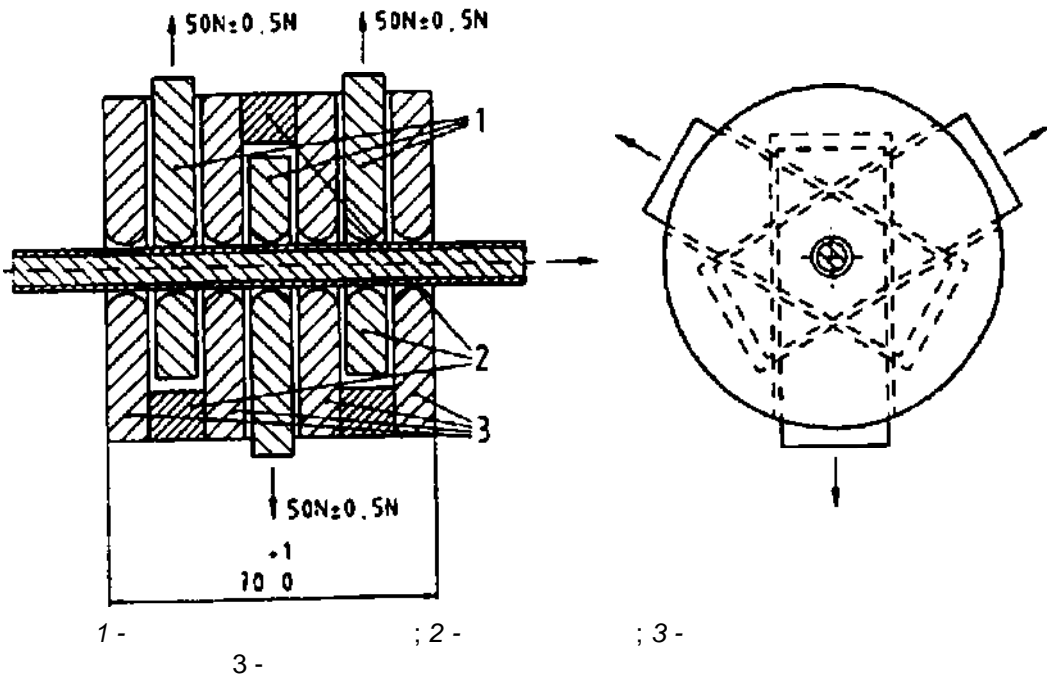
5.5.3

()

5.5.4
5.5.4.1
10

10

120* (3).



5.5.4.2

12

16 -

12 *

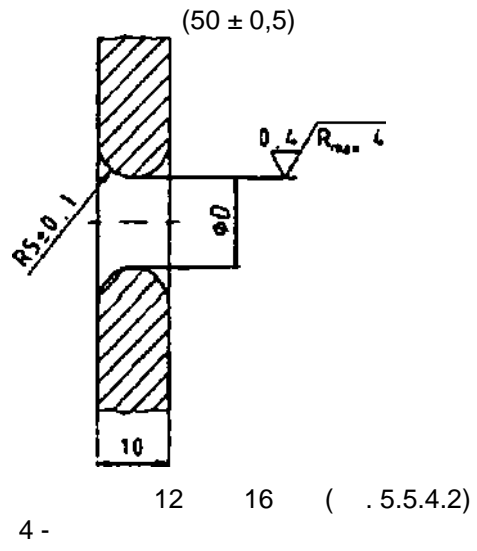
12,1 16

5.3.

5

R_{max} 4 R_a (0,4 4).

()



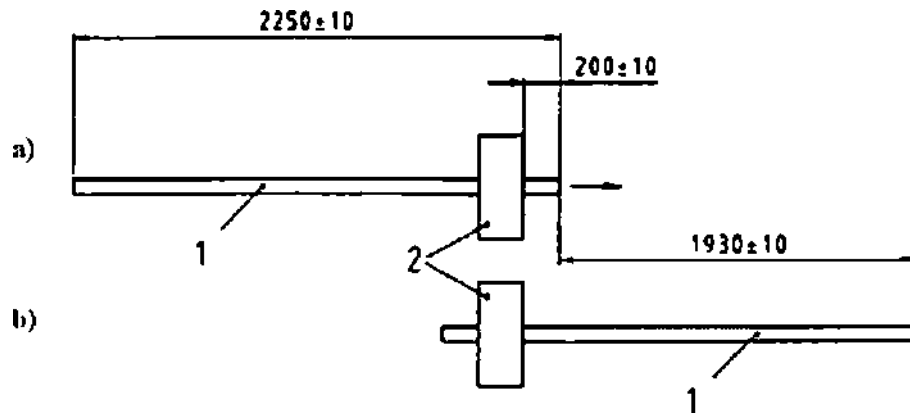
5.5.5
5.5.5.1

5.5.5.2

10)

(5).

(200 ±



a) -
b) -

1 - ; 2 - (3)
5 -

5.5.5.3 (50 1 0,5)

(0.5 ± 0.2) / (1930 ± 10)

5.5.5.4

5.5.5.5

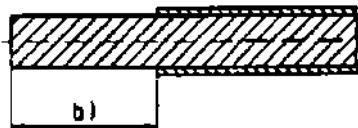
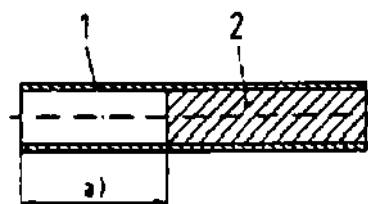
5.5.6

(6). V

0,1 %

5\$, %.

—100%
1930



))
мещение оболочки (положительно;
ние оболочки (отрицательное;
1 – оболочка; 2 – сердечник

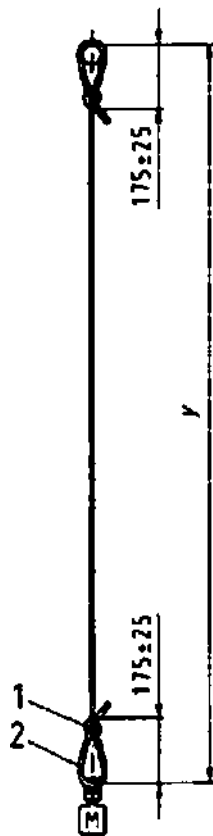
6 -

5.6
5.6.1

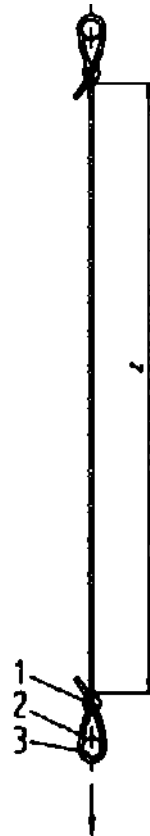
3000

5.6.2				
5.6.2.1				
5.6.2.2			(50 ± 0,1)	
5.6.2.3		5.6.2.2	(5 ± 0,5)	(1000 ± 1)
5.6.2.4	L_A	-	(100 ± 0,1)	
5.6.2.5		5.6.2.4	(150 ± 0,2)	
5.6.3	L_B		(5 ± 0,5)	
	(0,1 %)	($L_{fi} - 1$),	L_A
		$\varepsilon = 100\%$		
		L_A		
5.7	R			
5.7.1				3000
5.7.2				
5.7.2.1				
5.7.2.2			(10 ± 0,1)	
5.7.2.3		(1300)
		5.7.2.2	(60 ± 15)	(1000 ± 1)
	100			
		L_A		
5.7.2.4				
5.7.2.5		()
	(15 ± 5) °C	pH	5,5-8,0	(24 ± 0,2)
5.7.2.6	15			
5.7.2.7	5.7.2.1	5.7.2.2.		
		5.7.2.6	(60 ± 15)	5.7.2.3.
5.7.3	L_B			
	(0,1 %)	($L_A - L_3$).	1
		$R =$	100%	
		L_a		
5.8				S_p
5.8.1				3000
5.8.2				
5.8.2.1				
5.8.2.2			(10 ± 0,1)	
5.8.2.3		(1300)
		5.8.2.2	(60 ± 15)	(1000 ± 1)
	100			
5.8.2.4				
5.8.2.5	0,1			0,1

5.8.3					
5.8.3.1		S_p			
5.8.3.2					
5.8.3.3					
5.9					
5.9.1					
5.9.2					
5.9.2.1	364 (4.1.1.	4.4	4.6).	
5.9.2.2					
5.9.2.3					100
		4,95 - 5,05		$(100 \pm 0,1)$ 9.9 /	
5.9.2.4					
5.9.3		(100 ± 1)		(80 ± 1)	
5.9.3.1					4000
5.9.3.2					7),
			5.9.3.3.		
5.9.3.3					7),
5.9.3.4			5.9.3.2	5.9.3.3,	
(
)	(80 ± 1)		(175 ± 25) 7]].		(100 ± 1)
5.9.3.5			7).		
80			2000	100 $*10$	



) (.5.9)



) (.5.10)



) (.5.9)

1 - ; 2 - ; 3 - ;
 - (100 ± 1) ; z = 300 ; = 2000^{10°} (.5.9.3); -
 (80 ± 1) (.5.10.2)

7 -

5.9.4
 5.9.4.1

5.9.3, 10

(.5.2).
 100

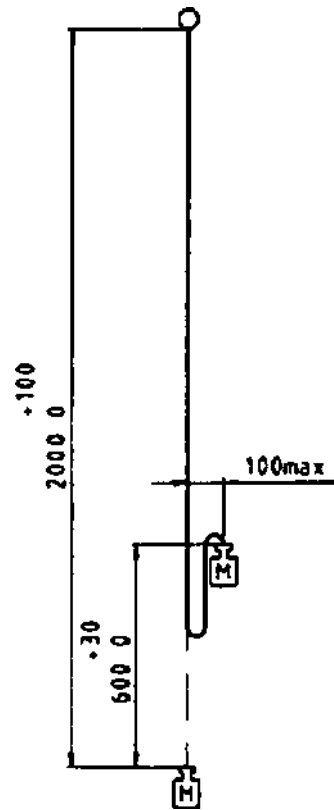
5.9.4.2

5.9.4.3

600²⁰

80
 60¹⁰ .
 100

(. 8).



$= (100 \pm 1)$
 $= (80 \pm 1)$

8 -

(. 5.9.4)

5.3.4.4

5.9.4.5

0.1

5.9.4.6

1

5.9.5.1.

5.9.5.2

(3 ± 0.5)

5.9.5

5.9.5.1

100

80

100

(. 9).

5.3.5.2

5.9.5.3

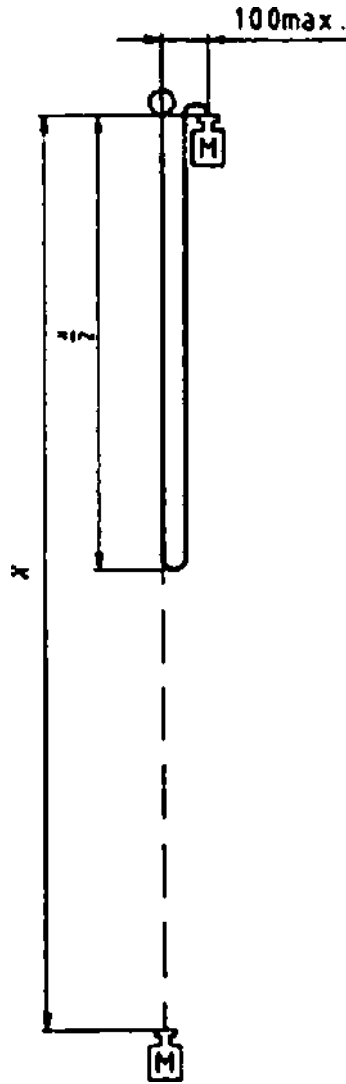
1

5.9.5.4

(3 ± 0.5)

5.9.5.5

5.9.5



9 - 5.9.4;
 = (100 ± 1) ;
 = (80 ± 1) (. 5.9.5)

5.10
 5.10.1
 5.10.1.1
 5.10.1.2
 5.10.1.3

EN 364 (4.1.1).
 - 364 (4.1.2.2).
 (15 ± 1) (20 ± 1)

3000
 5.10.2
 5.10.2.1
 5.10.2.2

5.10.2.3.

5.10.2.3

5.10.2.2,

5.10.2.4

300

7)].

5.10.3

5.10.3.1

5.10.2,

5.10.3.2

(.4.12.2).

5.10.3.3

3

6

6.1

- EN 365, 6.2 6.3.

6.2

a)

4.2. , 11,0: 9.2;

b)

6.3

1000

a)

b)

c)

d)

(), ()

701.

6.3,

7

EN 365 ,

a)

(), ()

b)

D

4.2;

c)

4.4;

d)

S_s 4.5;

e)

S_p

4.8;

4.9;

)

4.7;

h)

R

4.6;

i)

4.12.1 4.12.2;

J)

k)

l)

-) , ; /
 -) , ;
 -) , , ; , ;
 - , ;
 - , ;
 - q) , , , , , , ; , ,
 -) , , ;
 - s) (;)
 - t) , ; (; , 10,5
 -) , ;
 - v) , ;
 - w) , ; ,
 - x) , , ;
 - y) , , , EN 892;
6. ,

()

.1

300

.2
.2.1

.2.2

.2.3

.2.4

.2.5

.3.1

.3.2

.3.3

20

.4

.4.1

.4.2 .4.3,

.4.2

.4.3

80 %.

(ZA)

EEC

89/686/

89/686/

Z .1

89/686/		
1.1	II	4 5
1.1.2		3.4, 3.5, 4.9, 4.10, 4.11, 4.12, 5.8, 5.9, 6.2, 6.3 7
1.3.2		4.8, 4.9, 4.11, 4.12, 5.8, 5.9 5.10
1.4		6 7
2.4		7
2.12		6
3.1.2.2		4 5

EFTA.

()

.1

364	-	•
365	•	×
701	-	•
919	-	×

614.895:614.821:620.1:006.354

13.340.99

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